

Simulation of the Landing of Rosetta Philae on Comet 67P/Churyumov-Gerasimenko



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Comets - tiny imposters

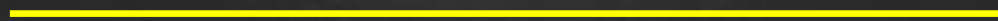
Hyakutake



Comet nucleus 81 P/Wild-2

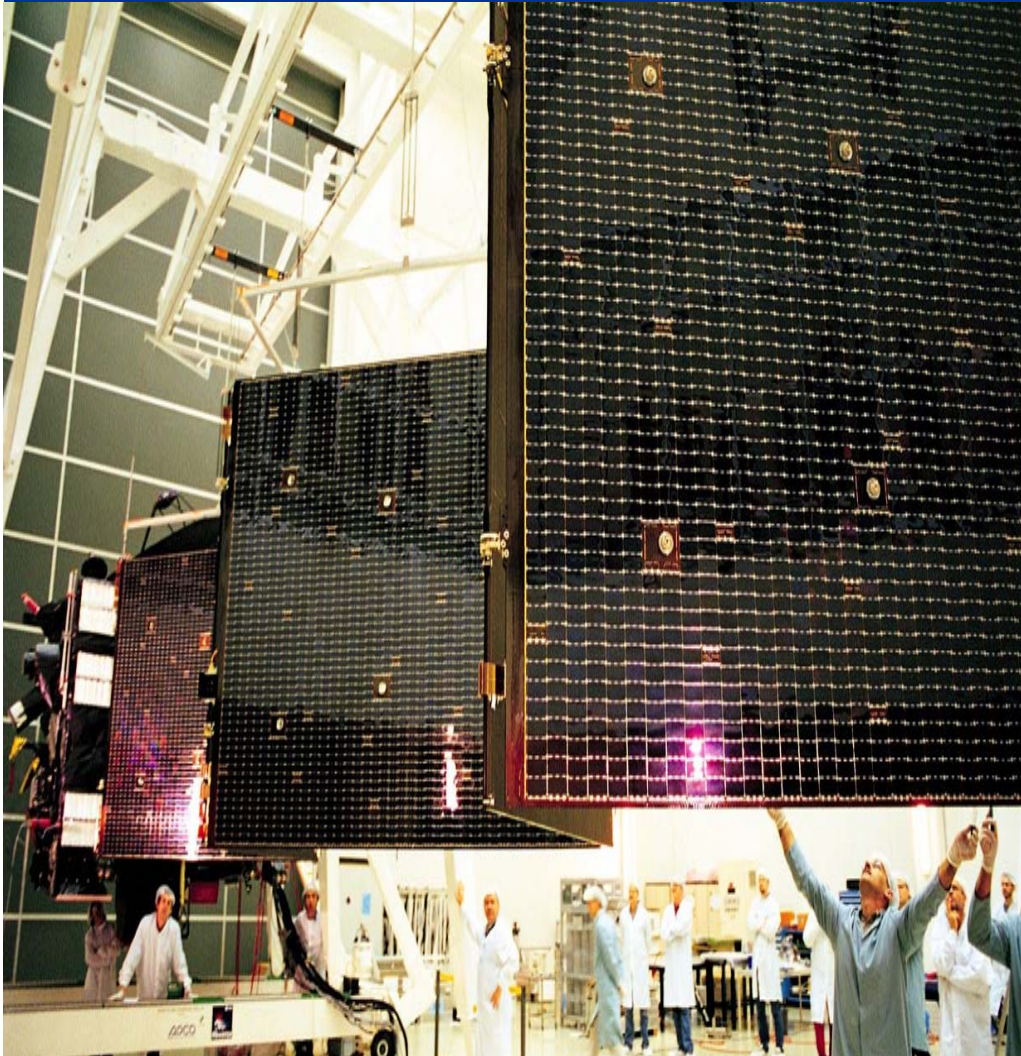


Stardust
2004



~ 5 km

Mission Rosetta: An ESA corner stone mission towards a comet nucleus



Mission Rosetta - fact sheet

Mass: 2.9 Tons (1.6 tons fuel)

Size: 3 x 2 x 2 m (solar cells,
32 m long)

costs: (in human resources)
about 15.000 years

Science payload:

150 kg on orbiter and

96 kg for the Rosetta Lander Philae

Rosetta orbiter
(hidden behind extended solar panels...)

Mission Rosetta: an ESA corner stone mission towards a comet nucleus



Selection of target comet for Rosetta mission....

Short timeline of mission:

start of hardware phase

cancelled launch towards comet 46P/Wirtanen

launched with new target comet, 67P/Churyumov-Gerasimenko

in orbit of comet

landing on comet nucleus

about 1996

Jan 2003

March 2004

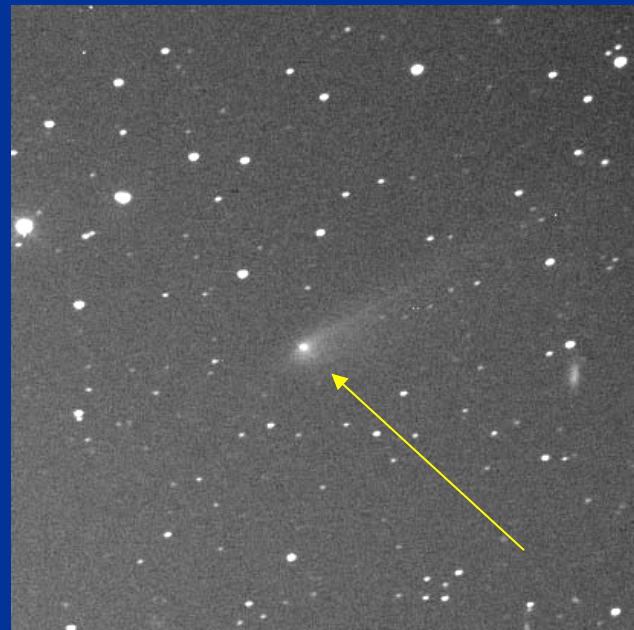
June 2014

Nov 2014

Selection of new target comet for Rosetta in 2003* :

New target comet: 67P/Churyumov-Gerasimenko

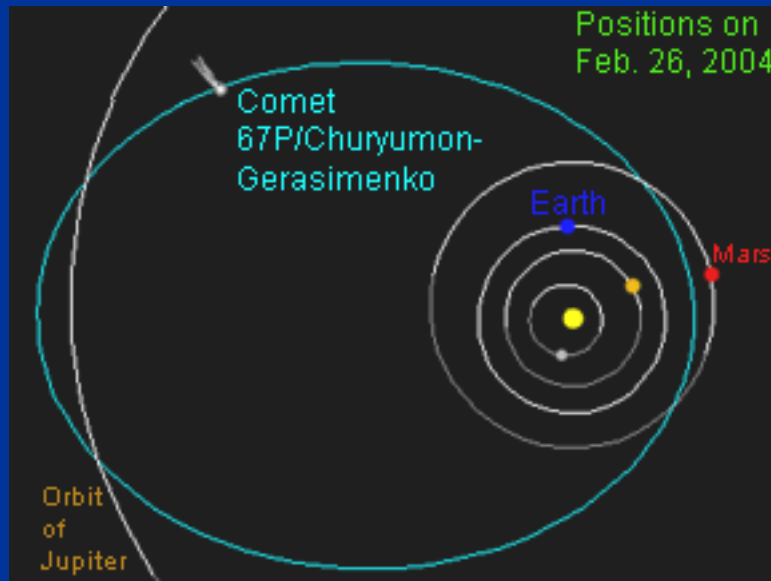
Description			periodic comet - (Jupiter family)
<u>nucleus size</u>	=		<u>3 x 5 km</u>
semimajor axis(a)	=		3.511 AU
eccentricity (e)	=		0.632
inclination (i)	=		7.1°
perihelion (q)	=		1.292 AU
aphelion (Q)	=		5.730 AU



* The 2003 launch was cancelled due to technical problems of Ariane V rocket system.

67P/Churyumov-Gerasimenko
February 1st 2003

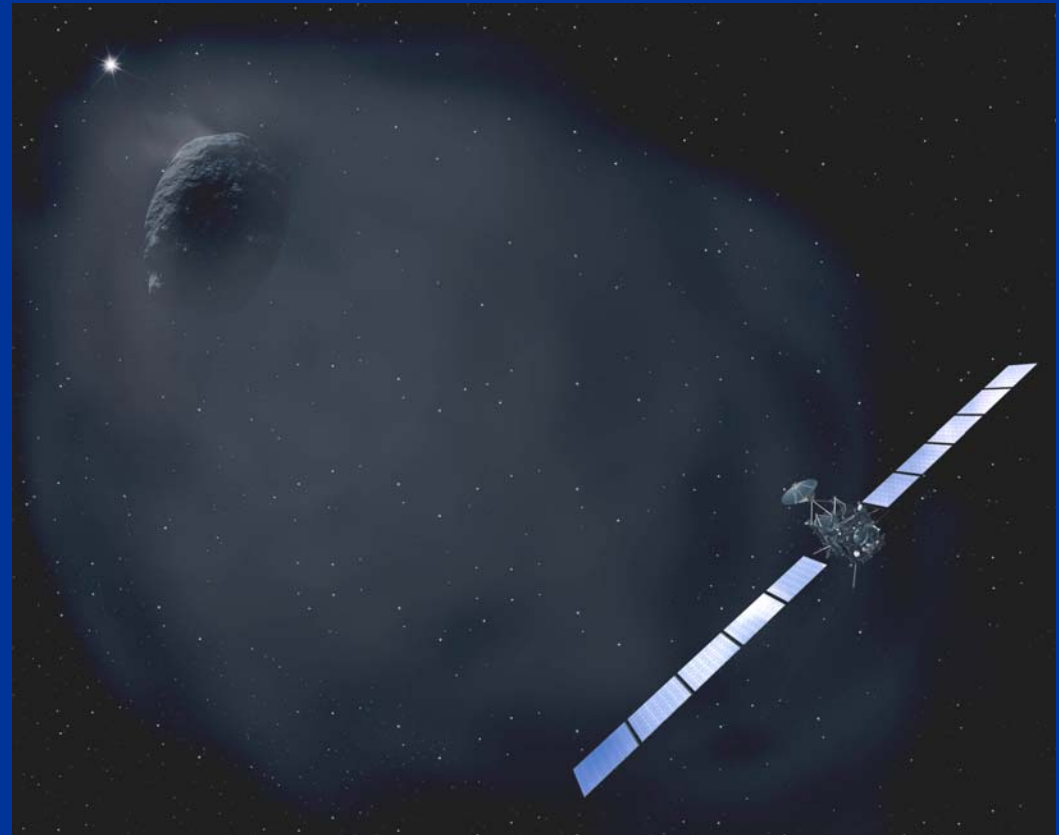
Approaching comet 67P/ Churyumov-Gerasimenko



Flight to the comet
(2004-2014: 10 years)

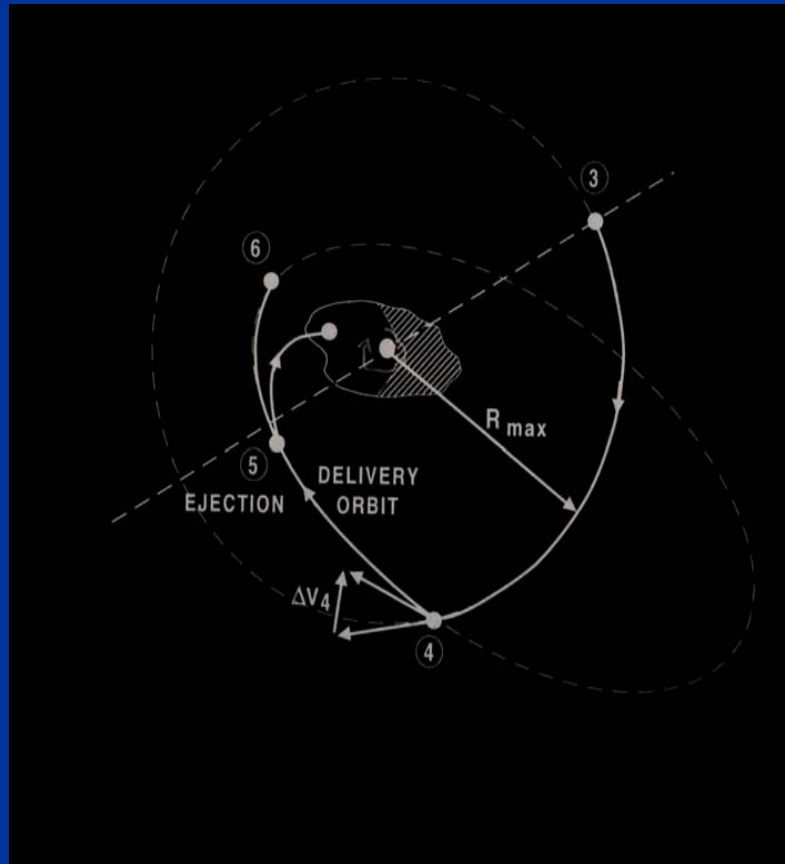


Launch
with Ariane V
2004

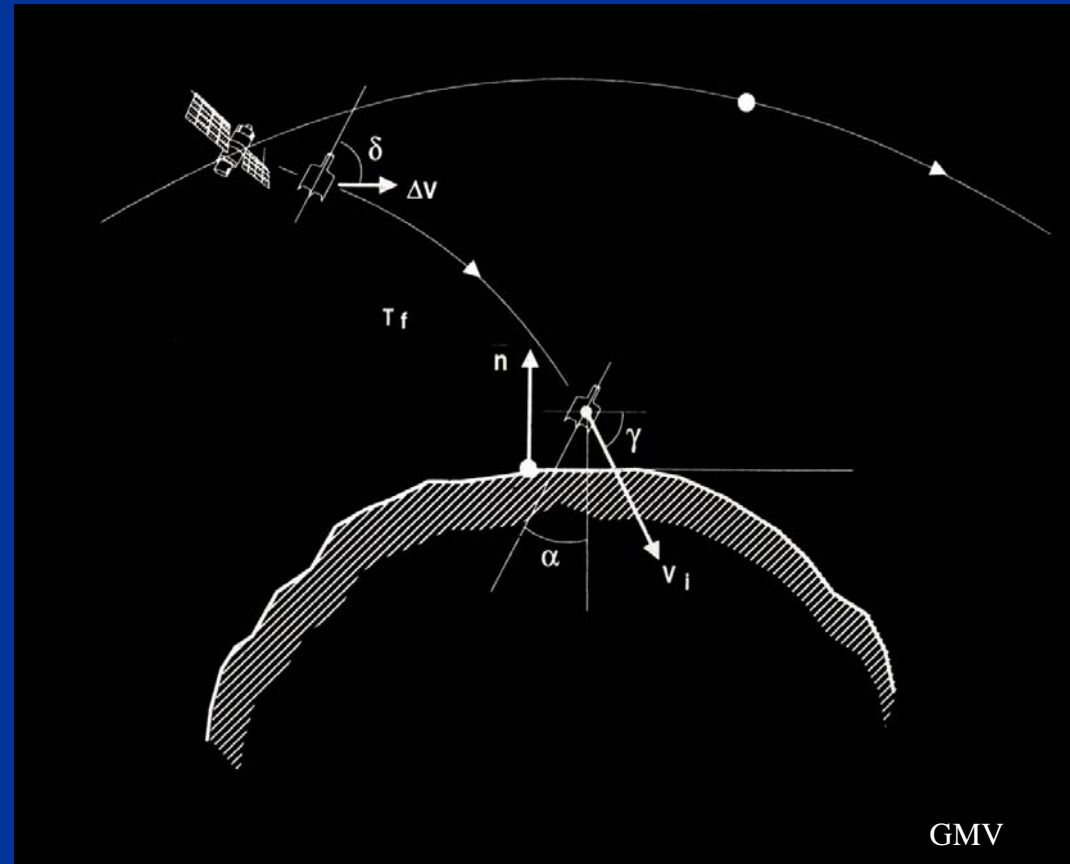


Comet mapping phase
(2014: 3 months)

Rosetta Lander - Mission Analysis



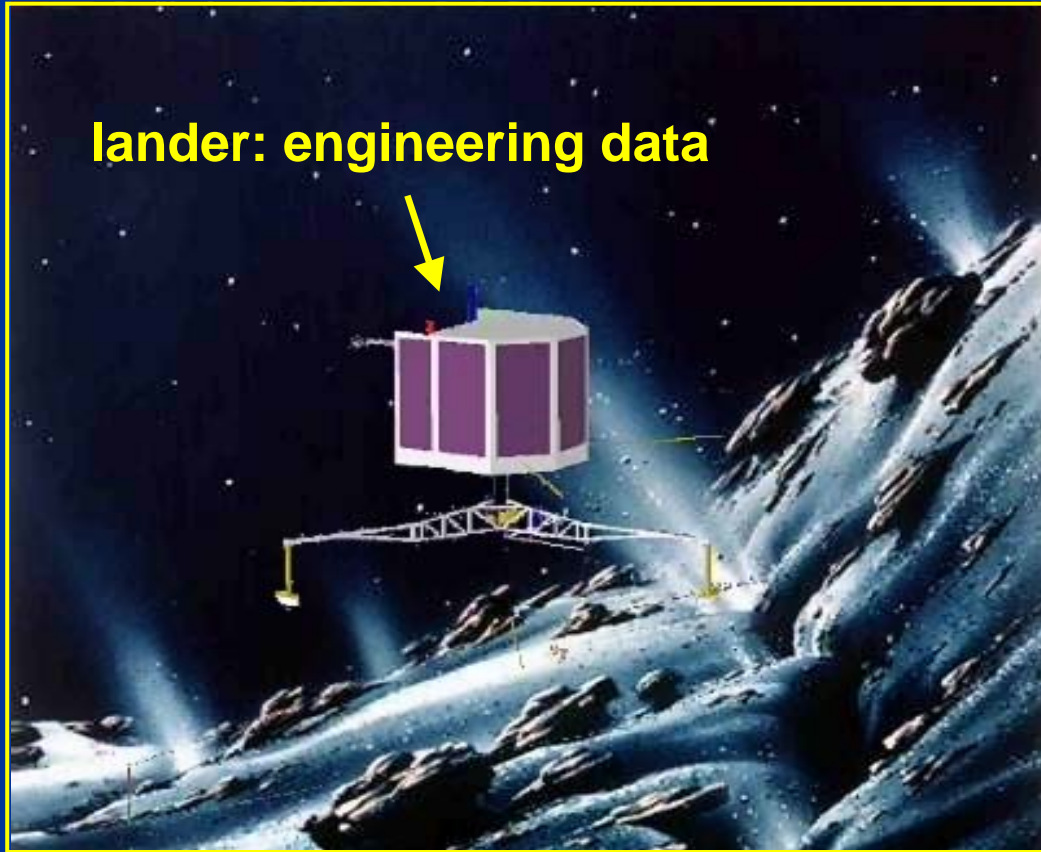
Orbiter maneuver:
Preparation for descent phase
(several days)



Orbiter, lander and comet:
Separation and descent
(about one hour)

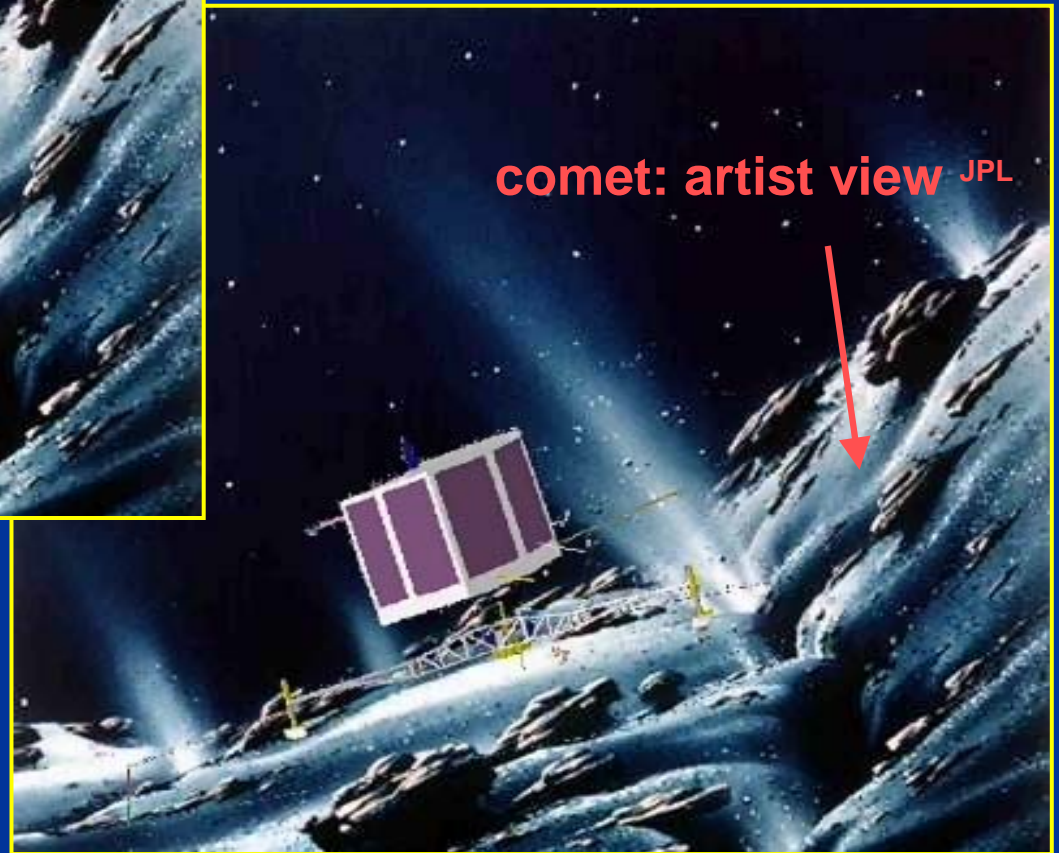
Rosetta Lander: Impact on comet

lander: engineering data



Lander and comet:
Touch down (sec)

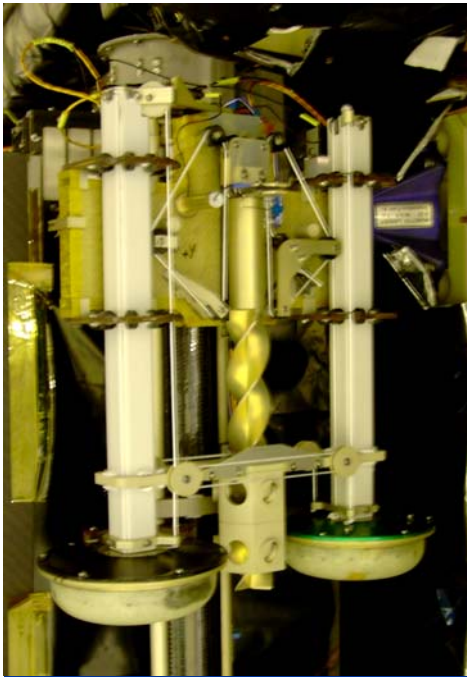
comet: artist view JPL



Rosetta lander Philae:

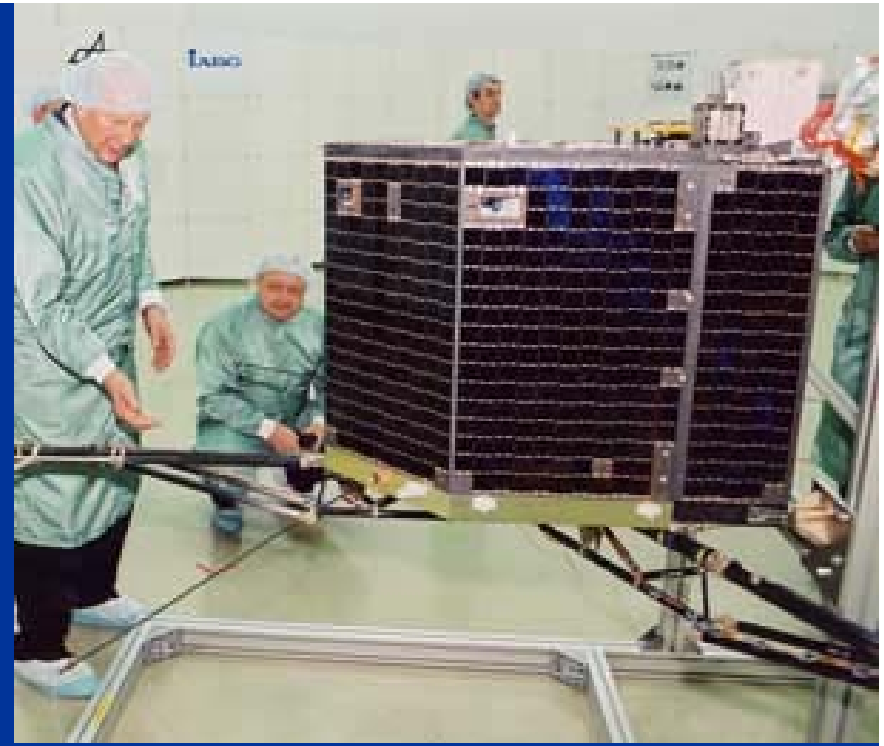
Hardware, simulation and qualification tests
concerning the impact on the comet nucleus:

lander flight hardware
concept of inelastic impact on comet surface
simulation model
comet surface
model parameters



Detail: Lander foot and icescrew

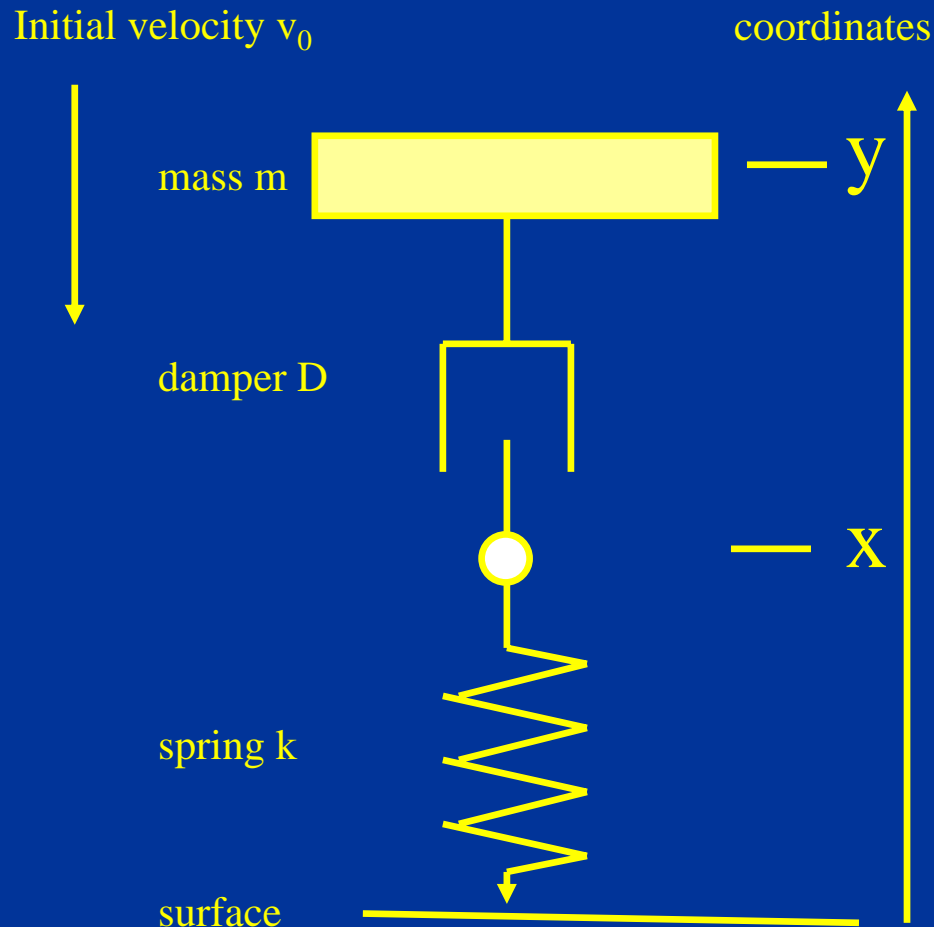
Lander Philae - flight hardware



Rosetta Orbiter
(Kourou 2003)



Simplified 1-D models for inelastic impact on comet surface



without spring (elasticity k indefinite)

Velocity dependent damp force:

$$m\ddot{y} + D\dot{y} = 0$$

$$v(t) = v_0 \cdot \exp(-D/m \cdot t)$$

$$s(t) = v_0 \cdot 1/(D/m) \cdot (1 - \exp(-D/m \cdot t))$$

with spring

coordinates: x , y and $d = y - x$

forces along coordinate axis are equal:

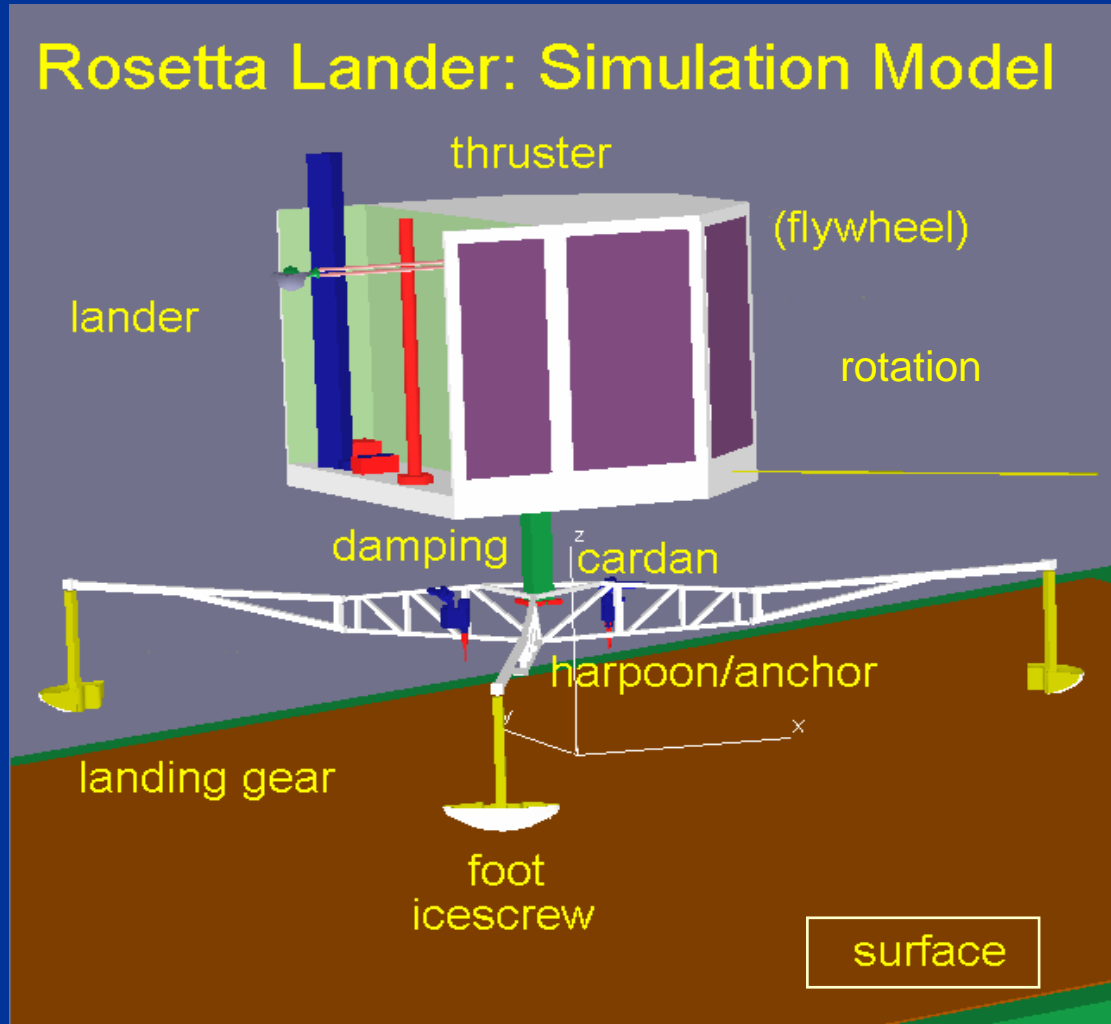
$$m\ddot{y} = -D\dot{d}$$

$$D\dot{d} = -kx$$

condition for inelastic impact
(no rebound)

$$\tau_{\text{spring}} < \pi/2 \cdot \tau_{\text{damper}} \quad \text{or} \\ k > 4 D^2/m$$

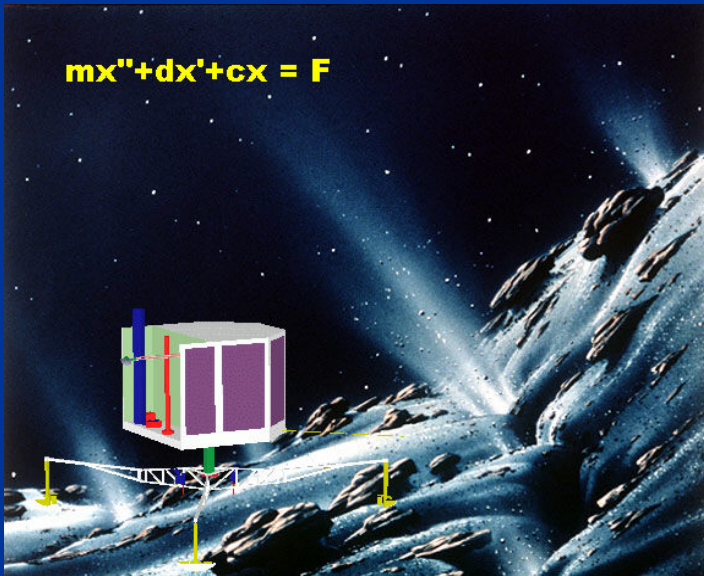
Simulation of Rosetta Lander 3-D Dynamics



Rosetta Lander Model Dynamic Parameters:
Source : Lander and Lander documentation
(theory and measurement)

Elements of Dynamics: Interaction with the comet surface

$$m\ddot{x} + d\dot{x} + cx = F$$



Lander

Hold-Down-Thrust

Flywheel

Damping

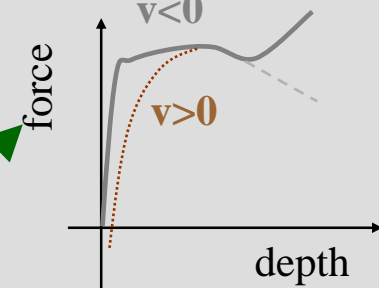
Elasticity

Cardan

Anchor

Landing Gear

comet surface:
force diagram



friction

surface $F \sim \mu \cdot F_{\text{normal}}$

Kelvin or Maxwell
elements

Selected Landing Site
(not to scale !)

Numerical Simulation:

The numerical simulation makes use of detailed geometry, joints, mass allocation, inertia etc. as defined in Lander CAD design files/documents.

The very basic mechanical / dynamical properties of the lander - comet simulation system are:

Mass (lander)	$M = 96 \text{ kg}$
Inertia	$I = 5 \cdot 10^{-6} \text{ kg} \cdot \text{m}^2$
mass (landing gear)	$m = 9 \text{ kg}$
Momentum of flywheel	$L = 5 \text{ Nms}$
Damping tube	$d = 800\text{-}1200 \text{ Ns/m}$
Cardan joint friction	$t = \text{up to } 30 \text{ Nm}$
Landing gear rigidity per leg	$k = 1.3 \cdot 10^4 \text{ N/m}$

Impact velocity	$v \text{ nominal } 0.5 \text{ m/s}$ $< 1 \text{ m/s}$ $(1.1 \text{ to } 1.5 \text{ m/s})$
-----------------	--

Rotation of lander	$w = 0.4 \text{ }^\circ/\text{sec}^*$
Angle of attack α	17° ^*
Angle of impact β and g	$9^\circ \text{ (or } \beta^* = 81^\circ \text{)}^*$ 8° ^*

Gravity	$a = 5 \cdot 10^{-4} \text{ m/s}^2$ (10^{-3} m/s^2)
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Comet surface friction (assumption: prop. to impact force)	
foot	0.2^*
screw	1^*

Nominal forces due to foot	
up	up to $2 \cdot 10^5 \text{ N}^*$
down	0 N^*

Nominal forces due to ice screw (ice-pic)	
up	$F 1200 \text{ N}^*$
down	$F 1 \text{ N}^*$

* examples as used in most presentations
- red labelled: new target comet parameters

Test Examples

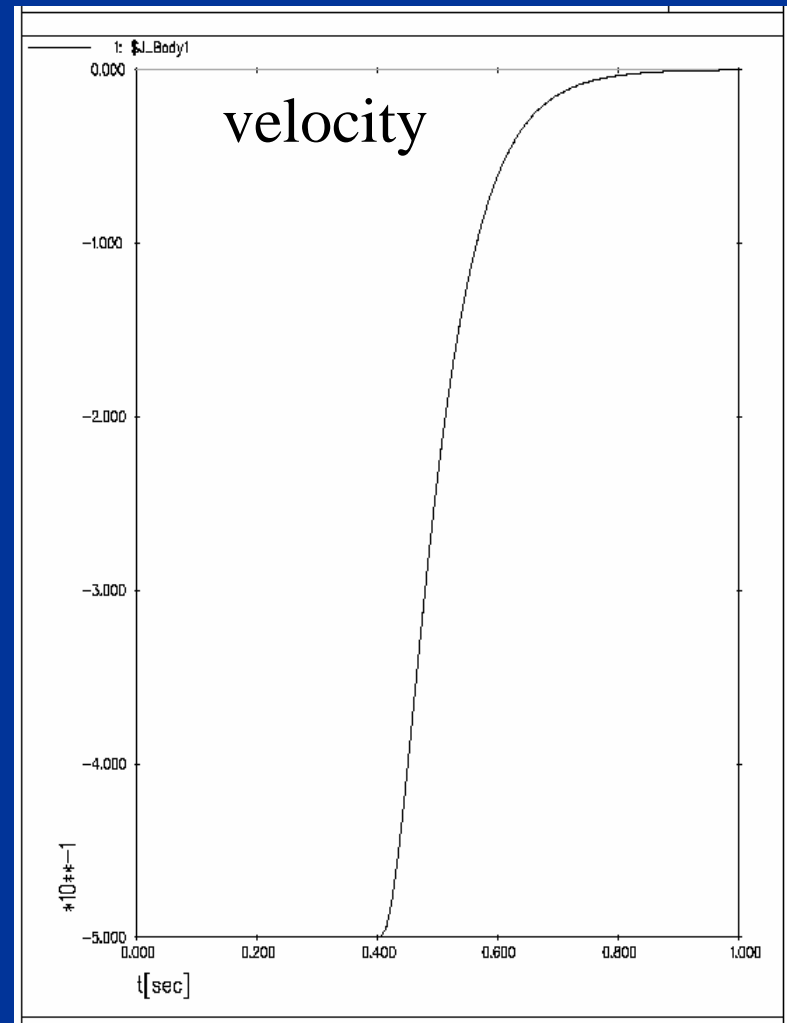
On-ground simulation and laboratory tests
in earth gravity environment:

Test of simulation model

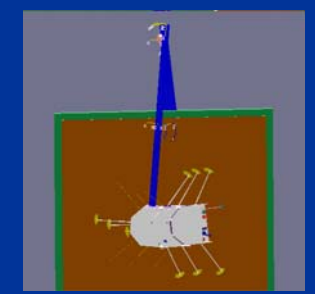
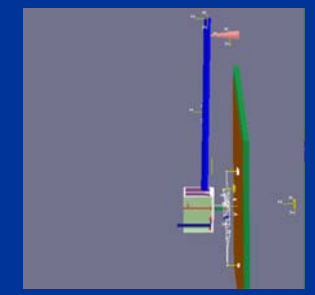
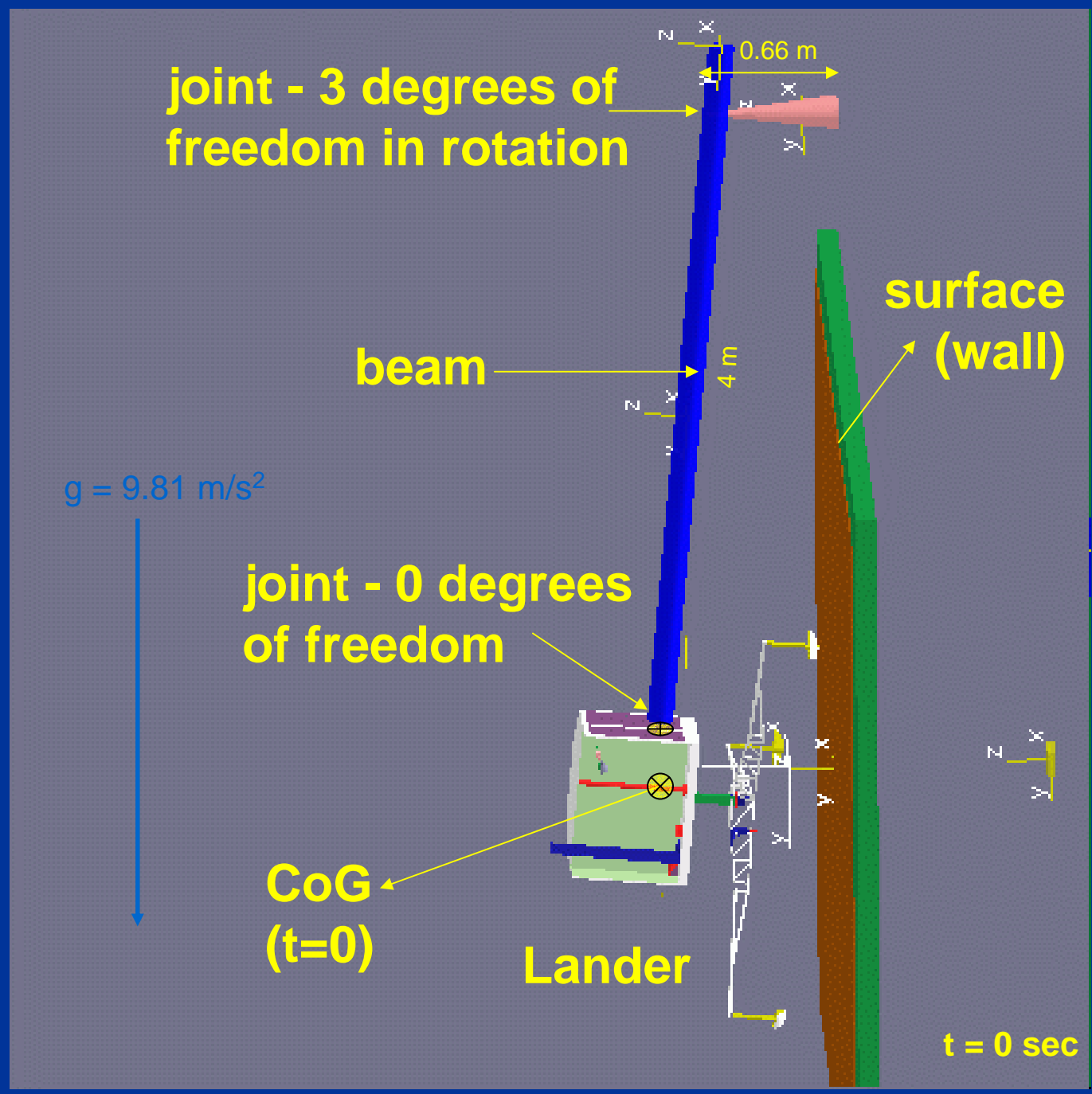
Damping Test (Cart)



Lindau, Jul 2001



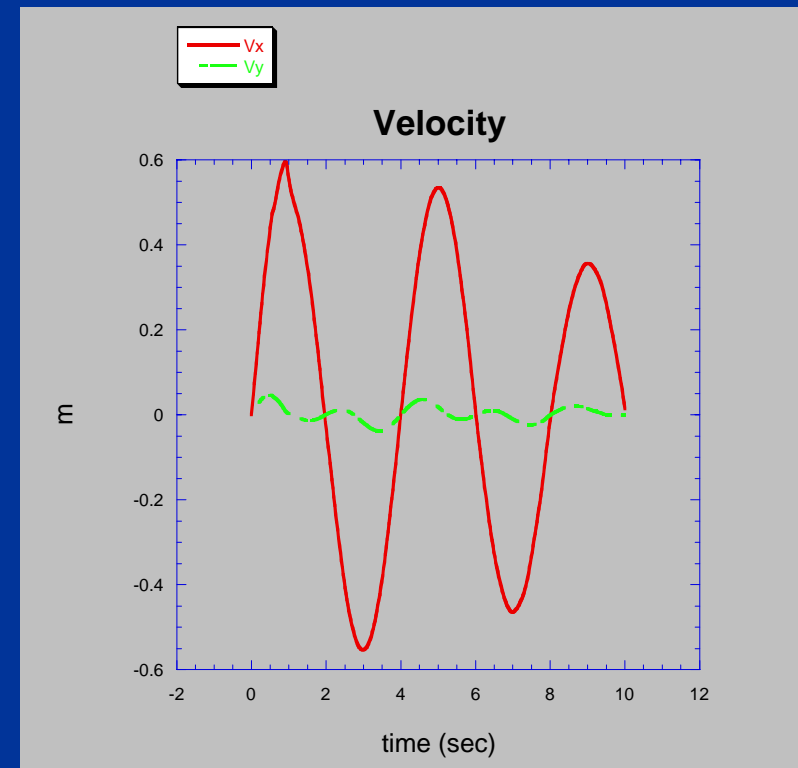
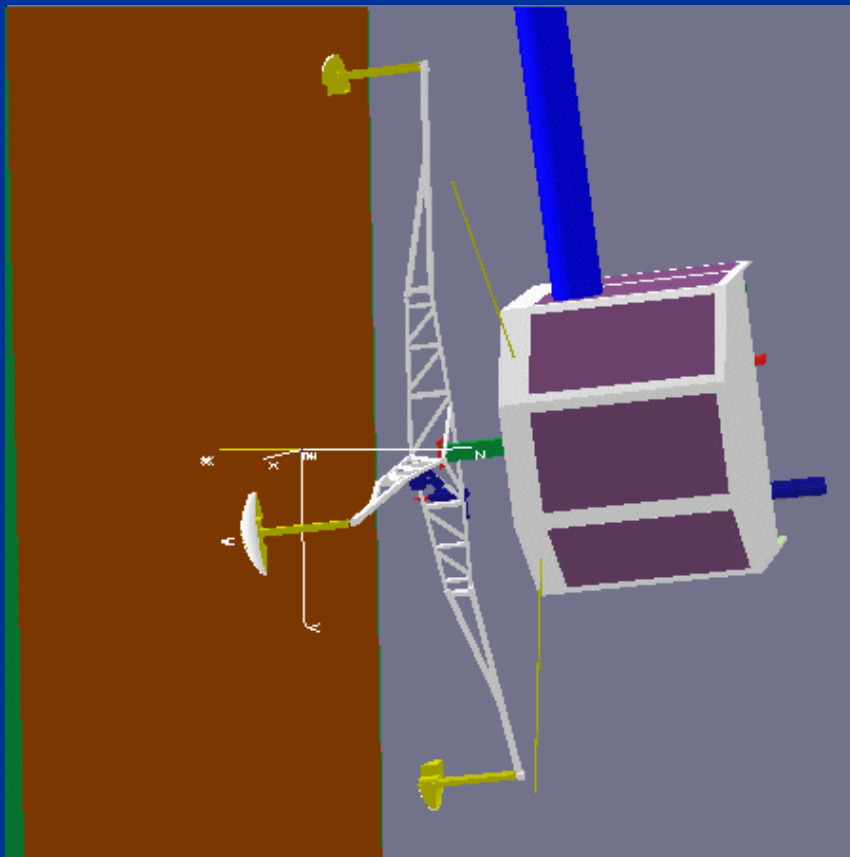
Test Configuration



$t = 0 \text{ sec}$

$t = \dots \text{ sec}$

Simulation test with pendulum in earth gravity environment (friction lander-wall: $m=0.1$)



Pendulum Test



Aluminium sheet surfaces



Comet analogue material

Lindau, Aug 2001

Simulation of landing scenario for 46P / Wirtanen*

nominal impact velocity:

0.5 m/s, 1 m/s maximum

gravity (comet)

$< 5 \cdot 10^{-4} \text{ m/s}^2$

landing concept:

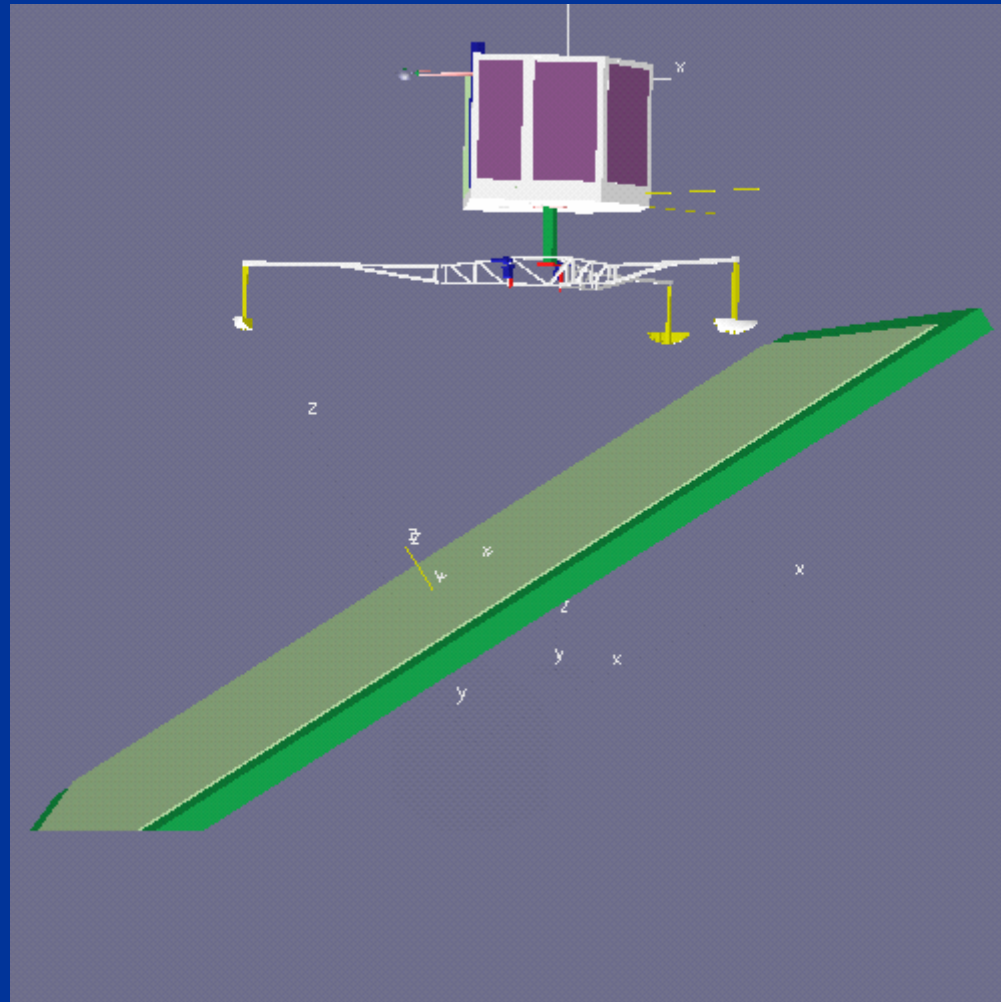
nearly torque free cardanic joint to limit the exchange of angular momentum between lander and comet

(about 18° free tilt angle, cardanic joint

friction torque about 10 Nm, adjustable up to 30 Nm)

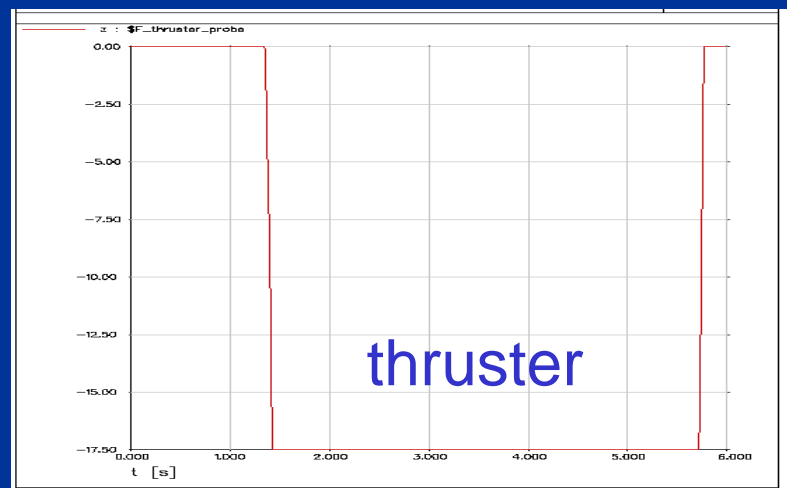
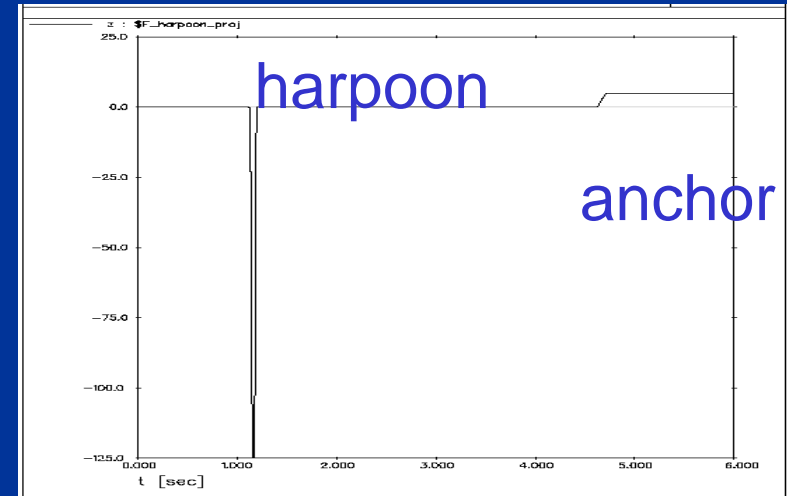
* valid comet mission target up to Jan 2003

Landersimulation I



(slow motion...)

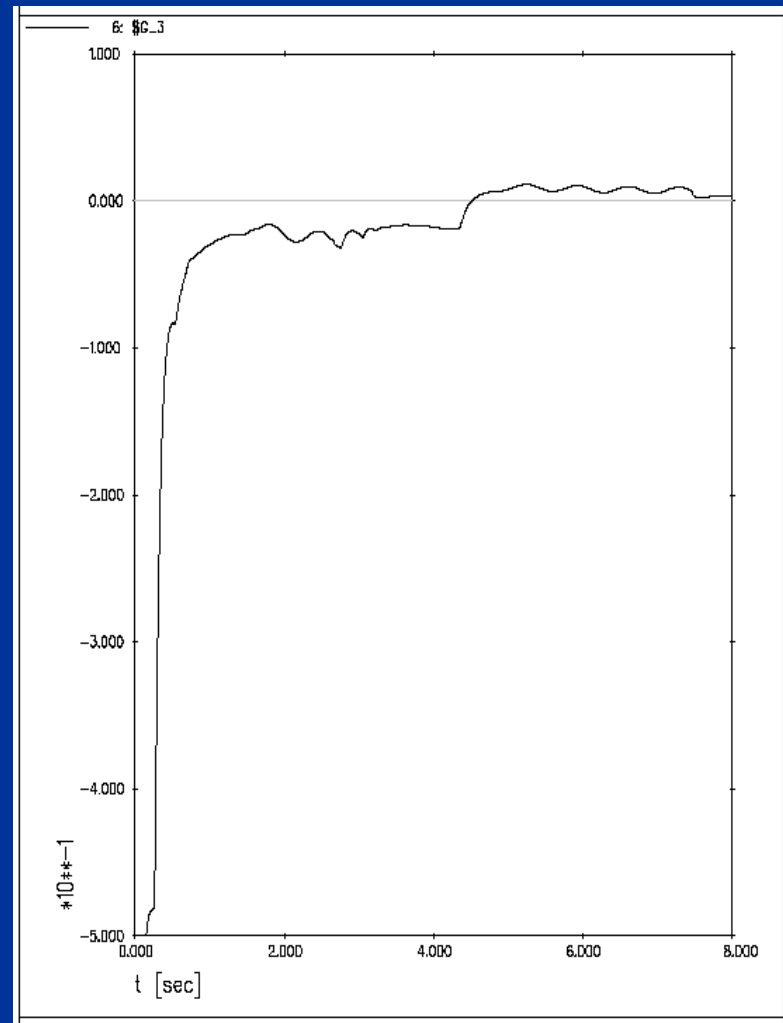
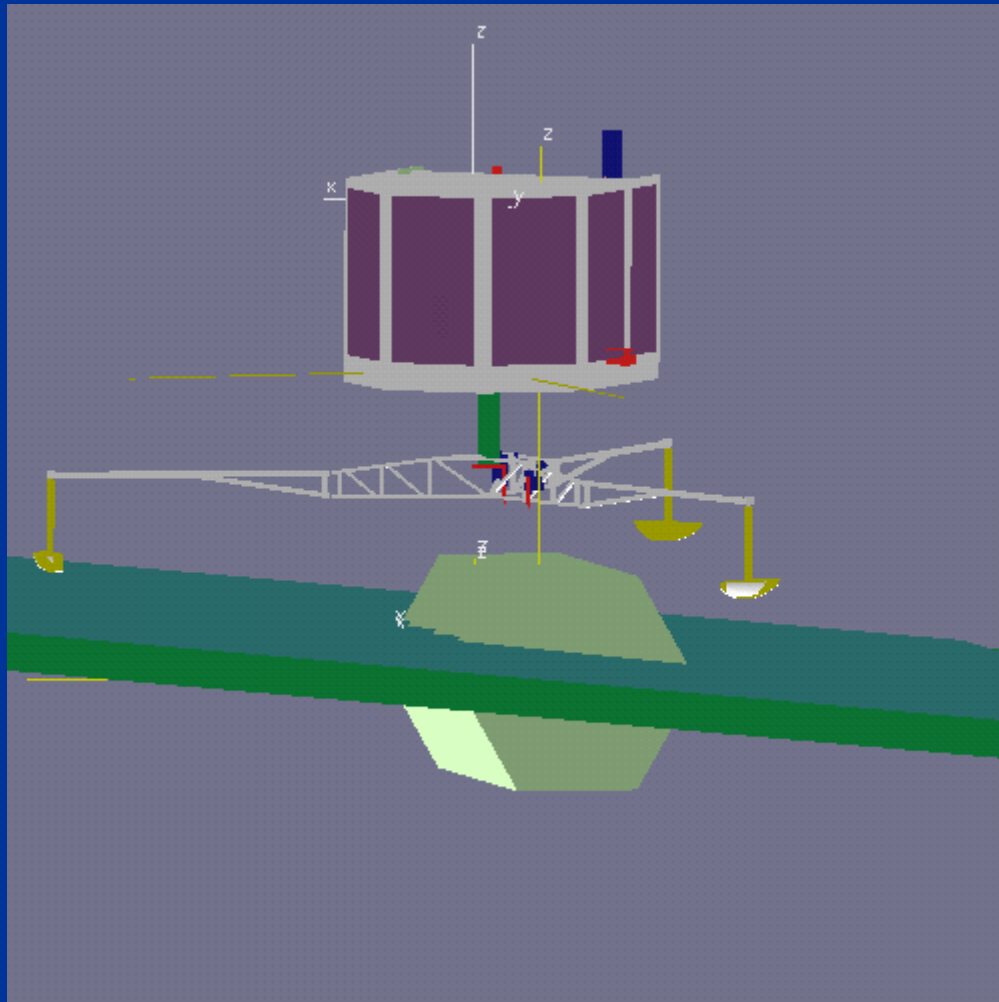
Impact velocity : 1 m/s



harpoon / anchor forces
and thruster force

Landersimulation II

Velocity (v_z , $v_z(t=0) = 0.5$ m/s)



New comet target: 67P/Churyumov-Gerasimenko

The new target has an observed radius of about 2 km (instead of 800 m as for 46P/Wirtanen) and the gravity is to about 10^{-3} m/s^2 . Therefore the impact velocity of the lander due to the free fall towards the comet is increased significantly.

Challenge:

adaptation of landing scenario towards increase impact velocity (increase from nominal $v_{\text{impact}} = 0.5 \text{ m/s}$ to **1.1...1.5 m/s**).

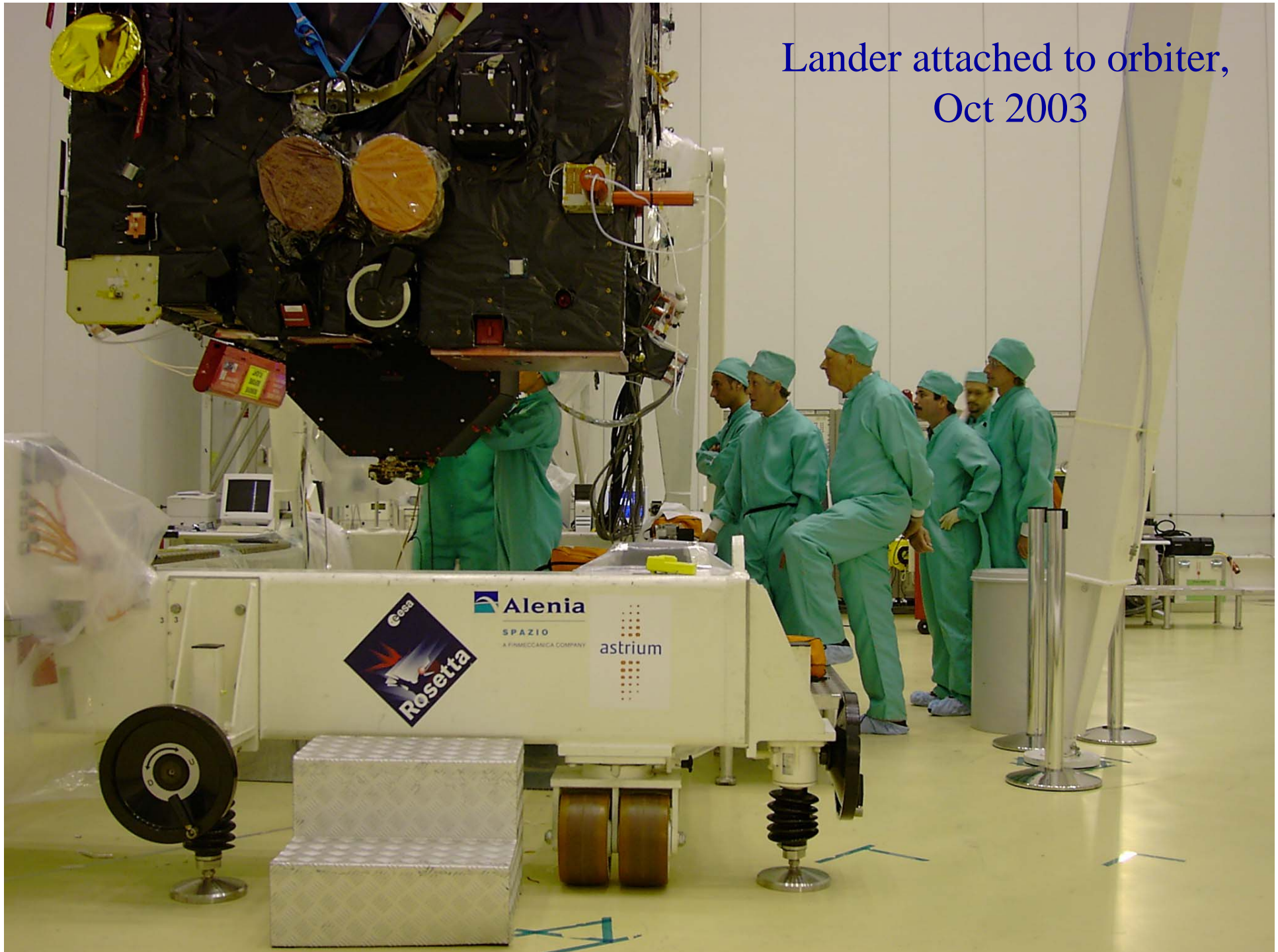
The kinetic energy of the lander is increased by a factor of up to 9.

Boundary condition:

Lander is mounted to orbiter, fully tested and qualified.

No major alterations are possible.

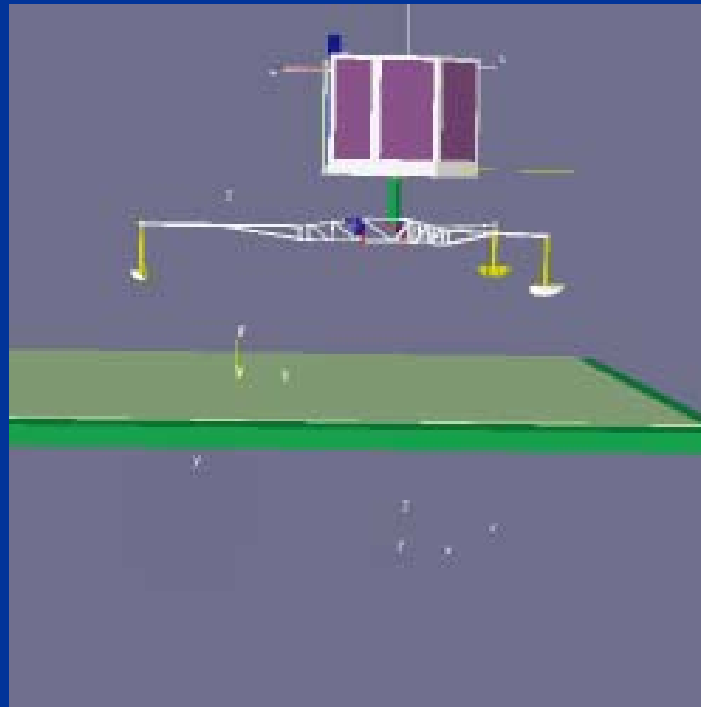
Lander attached to orbiter,
Oct 2003



Landersimulation III

$$V_z = -1.5 \text{ m/s}, V_x = 0.1 \text{ m/s}, V_y = 0.1 \text{ m/s}$$

“Flat surface”



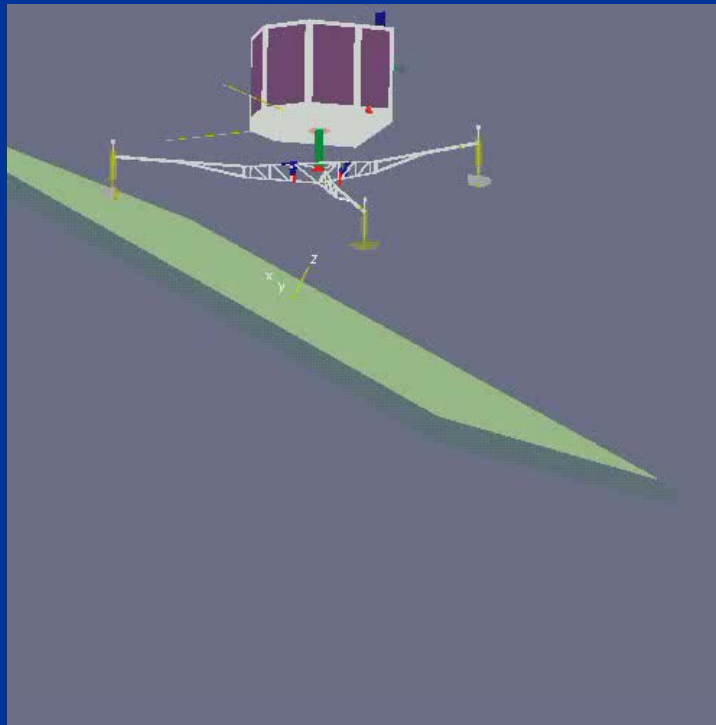
File b001

Landersimulation IV

$$V_z = -1.2 \text{ m/s}, V_x = 0.1 \text{ m/s}, V_y = 0.1 \text{ m/s}$$

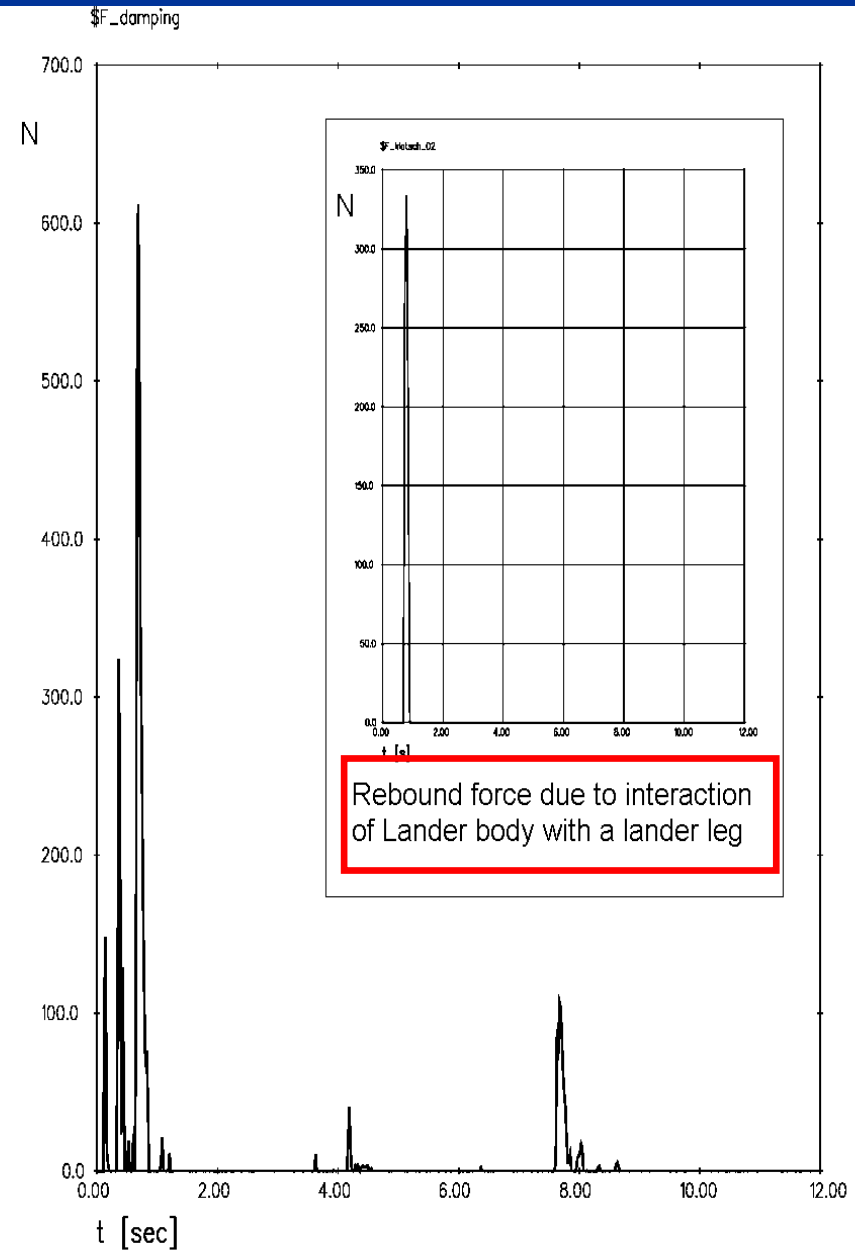
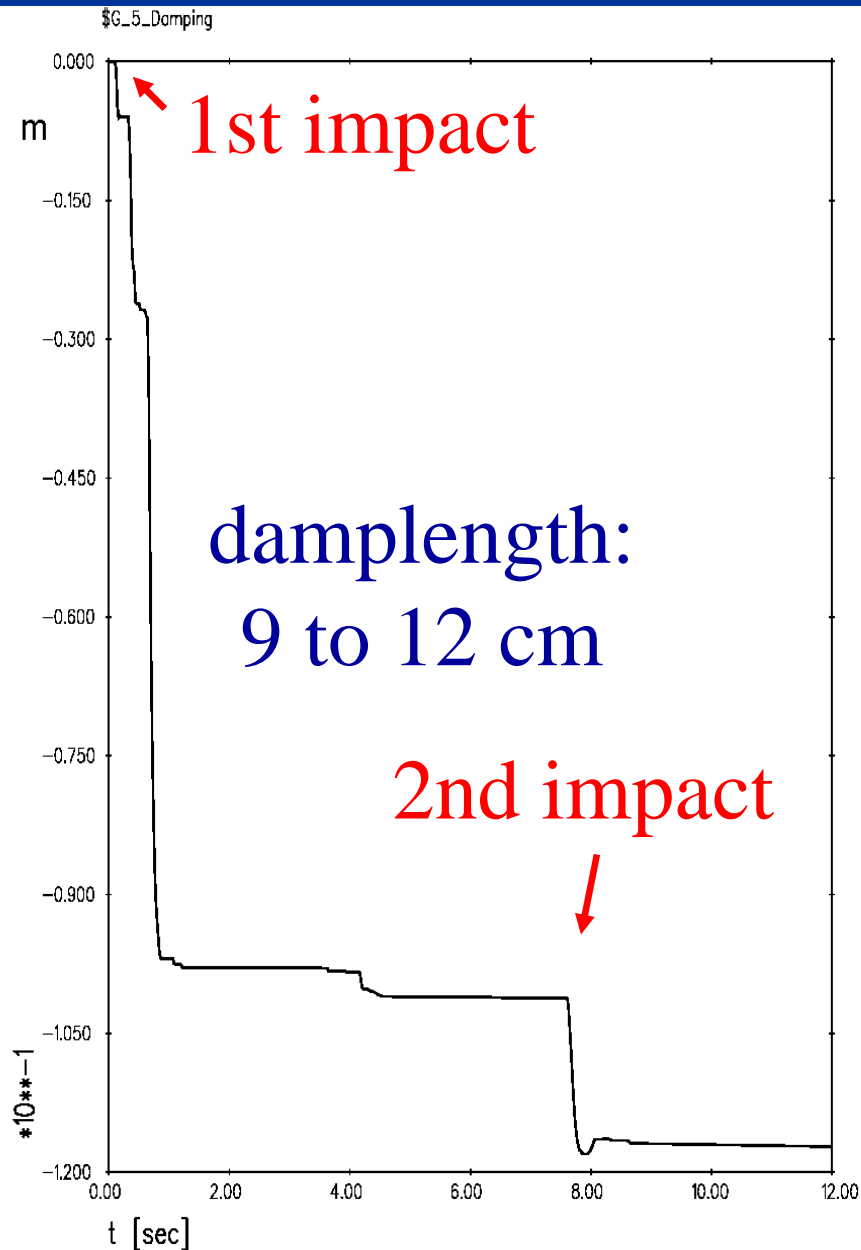
Cardanic joint stiffness: 520 Nm/rad

cardanic joint friction break torque : 30 Nm

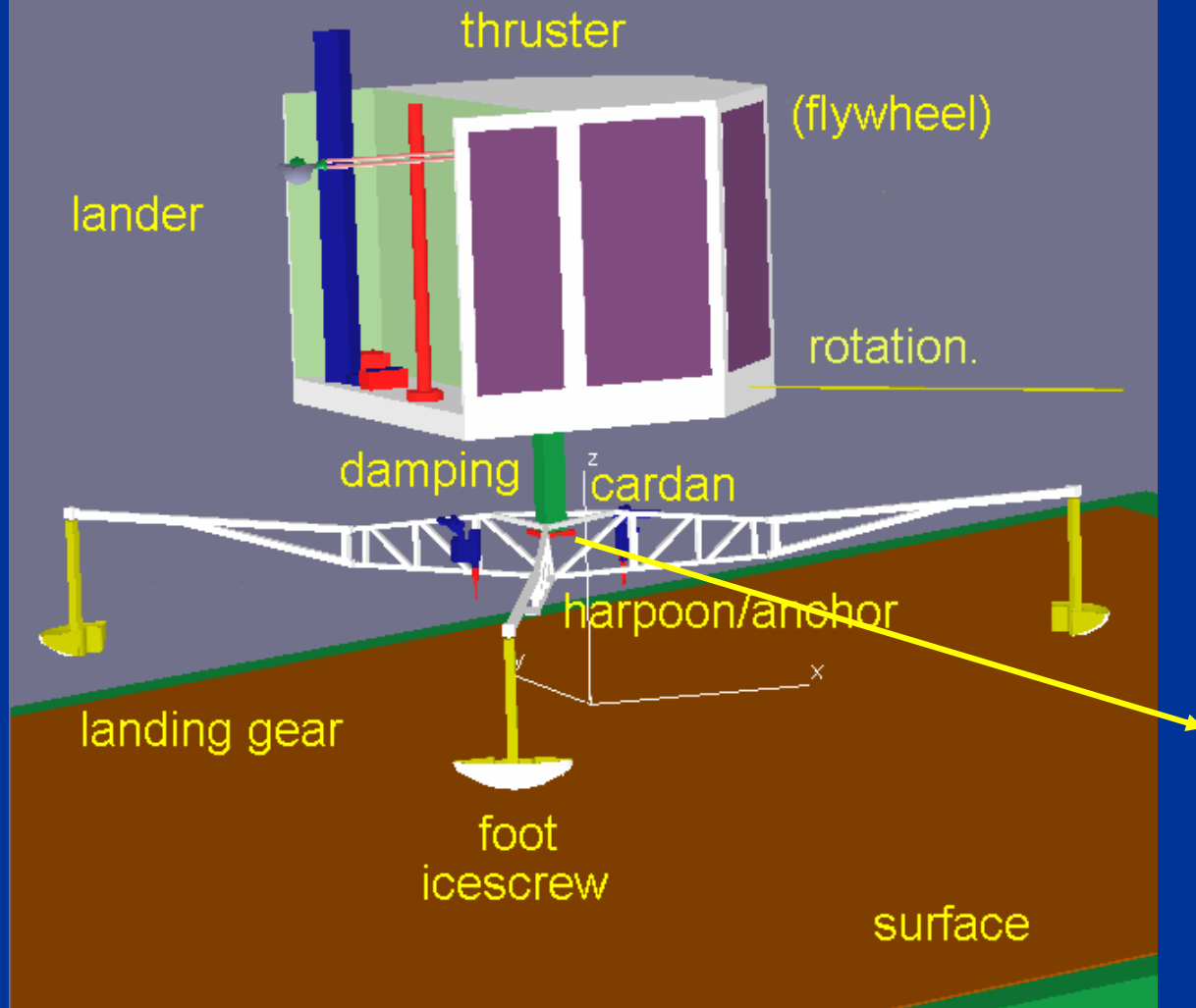


File 011

No cardanic joint tiltlimiter



Rosetta Lander: Simulation Model



Stiffness
cardanic joint
(not the friction
torque !):
520 Nm/rad
measured

Introduction of a tilt limiter to the cardanic joint:

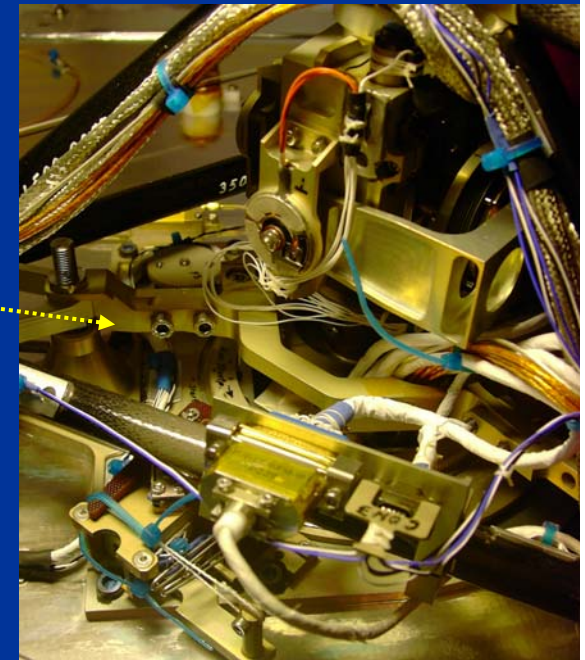
Limitation of free cardanic joint movement to 3° :

Advantage: The lander body can not touch the legs. Possible full use of damping length (about 18 cm) allows to damp impact velocities up to 1.2 - 1.3 m/s (function of slope).

Drawback: The angular momentum exchange with comet must be compensated by thruster and anchor action.



“free” cardanic joint

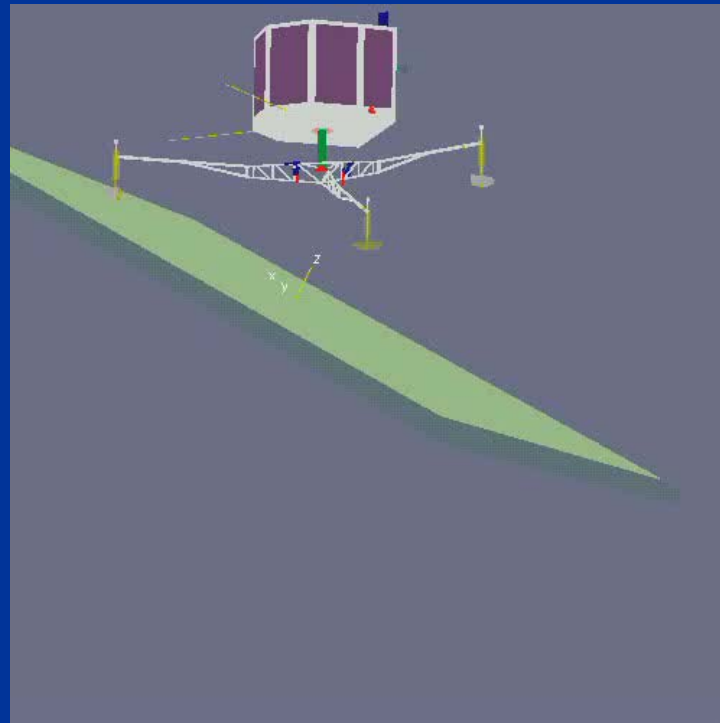


and with tilt-limiter

Landersimulation V

$$V_z = -1.2 \text{ m/s}, V_x = 0.1 \text{ m/s}, V_y = 0.1 \text{ m/s}$$

cardanic joint tilt limiter : 1000 Nm/rad ($18^\circ \rightarrow 3^\circ$)
cardanic joint friction break torque : 30 Nm



File 010

with cardanic joint tilt-limiter

